

TITLE OF INVENTION
CO-EXTRUDABLE MULTI-LAYER POLYMER

5 This application claims the benefit of U.S. Provisional Application No. 60/434,542, filed December 19, 2002, which is incorporated by reference herein for all purposes as if fully set forth.

BACKGROUND OF THE INVENTION

10 Field of the Invention.

 This invention relates to multi-layer polymer compositions that comprise two outer layers and an adhesive tie layer. This invention specifically relates to a multi-layer polymer composition comprising a polar polymer, e.g. polyvinylchloride (PVC), as the first outer layer, a non-polar
15 polymer, e.g., polypropylene, as the second outer layer, and a unique blend of polymers for the adhesive tie layers that allows the composition to be easily and advantageously coextruded.

Description of Related Art.

 It is often desirable to adhere polar polymers to non-polar polymers.
20 Non-polar polyolefins, such as polyethylene and polypropylene, have traditionally been available at a lower cost than polar polymers. Using the non-polar polymer for the bulk of a fabricated part, with only a thin layer of polar polymer on the surface, can provide attributes of the polar polymer at an overall lower cost.

25 As a specific example, PVC siding used in the housing construction industry typically has poor dimensional stability. Because of its low glass transition temperature, T_g , and flexibility, it can expand and contract with swings in atmospheric temperature, which can be a problem when used as housing siding. To minimize this problem, only heat-reflecting, light colors
30 can be used.

 To overcome the problem of poor dimensional stability, the PVC can be combined with a thick substrate of polypropylene, and/or glass fiber-reinforced or filled polypropylene, which are stiffer at all temperatures and more dimensionally stable. This can reduce cost, also, since the more
35 expensive PVC can be a much thinner layer than that used in conventional siding. With the dimensional stability problem solved, darker color PVC's can also be used.

The problem remains, however, of adhering the polar polymer, e.g., PVC, to the non-polar polymer, e.g., polypropylene, in a structurally sound and cost-efficient manner.

5 Attempts have been made to solve this problem in the past. For example, U.S. Pat. No. 6,045,732 (Nakatsuji et al.), discloses a multi-layer molded article having a skin material layer of a vinyl chloride resin and a propylene resin core. They disclose an adhesive layer (A), used to combine the vinyl chloride resin and propylene resin core, containing two
10 layers, one layer (polyester resin and epoxy-group containing ethylene copolymer) bonded to the vinyl chloride resin, one layer (at least one copolymer selected from an ethylene copolymer and epoxy group-containing copolymer) bonded to the propylene resin core. Alternatively, adhesive layer (B), comprising an ethylene resin composition containing a
15 polybasic carboxylic acid and an epoxy group-containing copolymer, can be used. These multi-layer articles, however, must be formed by molding under heat and pressure to form the final multi-layer article. The adhesive layers are formed in advance in a separate step by, for adhesive layer (A), co-extruding the adhesive layer, or by powder molding, inflation molding or
20 extrusion, for adhesive layer (B).

BRIEF SUMMARY OF THE INVENTION

The invention herein provides a multi-layer polymer comprising

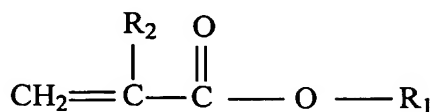
- 25 (1) a first outer layer,
 (2) a second outer layer and
 (3) an adhesive tie layer between the two outer layers,
 wherein the first outer layer comprises a polar polymer, the second outer layer comprises a non-polar polymer, and the adhesive tie layer
30 comprises
 (a) a copolyester elastomer that is totally or partially miscible with the polar polymer, (b) a non-polar polymer that is totally or partially miscible with the non-polar polymer in the second outer layer and (c) a copolymer that contains functional groups capable of reaction with the
35 functional end groups of component (a) and that is totally or partially miscible with the non-polar polymer in the second outer layer.

Component (c) of the adhesive tie layer preferably comprises an ethylene copolymer of the formula E/X/Y, wherein

E is the radical formed from ethylene and comprises about 40-90 weight % of the ethylene copolymer

X is the radical formed from

5



wherein R1 is an alkyl group with 1-8 carbon atoms,

R2 is selected from the group consisting of H, CH₃, or C₂H₅, and X comprises about 0-40 weight percent of the ethylene copolymer and

10 Y is selected from the group consisting of glycidyl methacrylate and glycidyl acrylate, and Y comprises 0.1-20 weight percent of the ethylene copolymer.

The multi-layer polymers can be advantageously used as exterior siding for buildings as well as other articles. Furthermore, the invention
15 provides processes for making a multi-layer polymer by coextrusion or by lamination.

BRIEF DESCRIPTION OF THE DRAWING(S)

FIGURES 1A and 1B represent a schematic drawing of the
20 coextrusion feedblock insert which allows three melt streams to converge and be coextruded.

DETAILED DESCRIPTION OF THE INVENTION

Definitions

25 The term "copolymer" means a polymer polymerized from two or more monomers, and thereby includes terpolymers, or more precisely, a polymer containing two or more repeat units.

The term "homopolymer" means a polymer polymerized from a single monomer in addition polymerizations, or from two monomers (e.g.,
30 one type of glycol and one type of diacid (or methyl ester of diacid)) in condensation polymerizations, or more precisely, a polymer containing one repeat unit.

The term "totally or partially miscible" can be explained as follows. The term "miscible" can be used to describe polymer-polymer blends with
35 behavior similar to that expected of a single-phase system. In most instances the critical property will be the glass transition temperature; a blend with a single glass transition temperature can be classified as "totally

miscible". With miscible polymer mixtures, mechanical compatibility is assured and a property compromise between the constituents is therefore achieved. The vast majority of polymer pairs, however, form two-phase blends after mixing, often evident from the small entropy of mixing for such very large molecules. These blends are generally characterized by opacity, distinct thermal transitions and poor mechanical properties. Usually, at least some mixing is observed at the polymer-polymer interface, resulting in a broadening of the two glass transitions, and these blends can therefore be considered "partially miscible."

Description

The present invention relates to a multi-layer polymer that is advantageously and easily formed by coextrusion. The invention overcomes the common problem of adhering a polar polymer to a non-polar polymer, and does so in a cost-effective and useful manner. The multi-layer polymer exhibits desired physical properties of the typically more expensive polar polymer, at a much lower cost than if the polar polymer was used alone. The resulting multi-layer polymer is useful in many ways, e.g., exterior siding for buildings, various construction materials, automobile interior parts, boat hulls and other marine parts, toys, etc.

The first embodiment of the invention provides a multi-layer polymer comprising (1) a first outer layer, (2) a second outer layer and (3) an adhesive tie layer between the two outer layers. The first outer layer comprises a polar polymer. The polar polymer is preferably selected from polyvinylchloride (PVC) homopolymer and copolymers, acrylonitrile-butadiene-styrene (ABS), polyvinylidene dichloride (PVDC), poly(ethylene terephthalate) (PET) homopolymer or copolymers, polyamides, polycarbonates, ethylene vinyl alcohol (EVOH) homopolymer and copolymers, acid copolymers, ionomers, liquid crystalline polymers, polyacetals, acetal copolymers and polylactic acid. PVC is most preferred as the polar polymer. The first outer layer is typically useful in a thickness range of about 2-10 mils (0.05-0.25 mm).

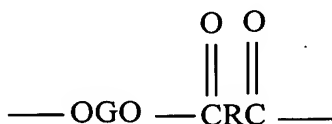
The second outer layer comprises a non-polar polymer. The non-polar polymer is preferably a polyolefin, and is more preferably selected from polypropylene homopolymer and copolymers, and polyethylene homopolymer and copolymers. The non-polar polymer is

most preferably polypropylene homopolymer with or without fiberglass or other mineral (e.g., talc) reinforcement.

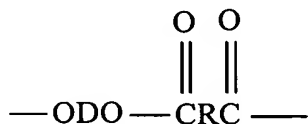
5 The adhesive tie layer comprises (a) a copolyester elastomer that is totally or partially miscible (see definition above) with the polar polymer, (b) a non-polar polymer that is totally or partially miscible with the non-polar polymer in the second outer layer, and (c) a copolymer that contains functional groups capable of reaction with the functional end groups of component (a), and that is totally or partially miscible with the non-polar
10 polymer in the second outer layer.

The copolyester elastomer preferred in the invention herein is available from E. I. du Pont de Nemours and Company (Wilmington, Delaware) under the trade name Hytrel® and is sold in various grades. Hytrel® is a thermoplastic ether-ester elastomer with properties of rubber
15 and the mechanical performance of plastics. The polyether segments of the elastomer are relatively soft, and the polyester segments are relatively hard. The amounts of each can be varied to achieve different properties. The polar nature of the copolyester elastomer allows for the property of partial miscibility with the polar polymer in the first outer layer.

20 More specifically, the copolyester elastomer comprises a segmented thermoplastic copolyester comprising a multiplicity of recurring long chain ester units and short chain ester units joined head-to-tail through ester linkages. The long-chain ester units are represented by the
25 formula



and the short-chain units are represented by the formula



30

where G is a divalent radical remaining after the removal of terminal hydroxy groups from a poly(alkylene oxide) glycol having a molecular

weight of about 400-6,000 and a carbon to oxygen ratio of about 2.0-4.3. R is a divalent radical remaining after removal of carboxyl groups from a dicarboxylic acid having a molecular weight less than about 300. D is a
5 divalent radical remaining after removal of hydroxyl groups from a diol having a molecular weight less than about 250. The short-chain ester units amount to about 15-95 percent by weight of the copolyester, and at least about 50 percent of said short-chain ester units are identical. The copolyester elastomer is further described in U.S. Patents No. 4,739,012,
10 3,651,014, 3,763,109, and 3,755,146, incorporated by reference herein.

Although not essential components of the copolyester elastomer, various amounts of any number of conventional fillers or compounding ingredients may be admixed. Examples of such ingredients include
15 various carbon blacks, clays, silica, alumina, calcium carbonate, titanium dioxide, glass fibers, antioxidants, antidegradants, tackifiers, processing aids such as lubricants and waxes, and plasticizers such as dialkylphthalates, trialkylmellitates, dialkyl esters such as dialkyl adipates, azeleates and glutarates, and polyester oligomers. The amounts used
20 depend, at least in part, upon the quantities of other ingredients in the composition and the properties desired from the composition. Also, minor amounts of other saturated and unsaturated polymers, such as alpha-olefins, may be added to reduce the cost or modify the properties of the composition.

Hytrel® 4069 and 4056 are high performance grades of
25 thermoplastic ether-ester elastomer preferred in the invention herein for the copolyester elastomer. They comprise soft segments of polytetramethylene glycol (PTMEG) and generally exhibit a shore D hardness of about 55 or less.

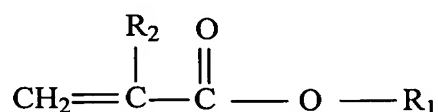
Component (b) of the adhesive tie layer is a non-polar polymer that
30 is totally or partially miscible with the non-polar polymer in the second outer layer. Component (b) is preferably a polyolefin, and more preferably polypropylene homopolymer or copolymer, or polyethylene homopolymer or copolymer. Most preferably, component (b) is the same non-polar polymer that comprises the second outer layer.

35 Component (c) of the adhesive tie layer comprises a copolymer that contains functional groups capable of reaction with the functional end groups of component (a) (i.e., hydroxyl and acid end groups) and that is partially or totally miscible with the non-polar polymer in the second outer layer. Preferred functional groups capable of reaction with the functional

end groups of component (a) include epoxy and anhydride functional groups. The preferred amount of epoxy functionality or anhydride functional groups is determined by trial and error by one skilled in the art.

5 Too much functionality could cause the copolyester elastomer to cross-link and make it difficult for the copolyester elastomer to flow through an extruder. Too little functionality and the copolyester elastomer will not react completely enough, leaving two phases without enough covalent bonding for proper strength.

10 Component (c) preferably comprises an ethylene copolymer of the formula E/X/Y, wherein E is the radical formed from ethylene, X is the radical formed from



15 wherein R1 is an alkyl group with 1-8 carbon atoms, R2 is selected from the group consisting of H, CH₃, or C₂H₅, or, alternatively, X is vinyl acetate, and Y is selected from the group consisting of glycidyl methacrylate and glycidyl acrylate. E preferably comprises about 40-90 weight %, X preferably comprises about 0-40 weight %, and Y preferably
20 comprises about 0.1-20 weight %, wherein all weight percentages are based on the total weight of the ethylene copolymer. More preferably, the E/X/Y copolymer is selected from the group consisting of copolymers of: ethylene-n-butyl acrylate- glycidyl methacrylate (EnBAGMA), ethylene – butyl acrylate – glycidyl methacrylate (EBAGMA), ethylene-glycidyl
25 methacrylate (EGMA), ethylene-methyl acrylate-glycidyl methacrylate (EMAGMA), ethylene –ethyl acrylate-glycidyl methacrylate (EEAGMA), ethylene – propyl acrylate – glycidyl methacrylate (EPAGMA), and ethylene - vinyl acetate - glycidyl methacrylate (EVAGMA). Most preferably the E/X/Y copolymer is EnBAGMA.

30 Component (c) may also preferably comprise an acid copolymer or anhydride derived from an acid copolymer. In that embodiment, component (c) more preferably comprises maleic-anhydride-grafted polypropylene.

35 As for the overall composition of the adhesive tie layer, preferably component (a) comprises about 25-65% by weight, component (b) comprises about 0-65% by weight, and component (c) comprises about

10-50% by weight, wherein all weight percentages are based on the total weight of the adhesive tie layer. More preferably, component (b) comprises about 25-65% by weight.

5 In a preferred embodiment of the multi-layer polymer of the invention herein, the first outer layer comprises PVC, the second outer layer comprises polypropylene homopolymer, and the adhesive tie layer comprises about 25-65% by weight Hytrel® 4069, more preferably about 30-46% by weight, most preferably about 38% by weight; about 0-65% by
10 weight polypropylene homopolymer, more preferably about 10-50% by weight and most preferably about 35-55% by weight; and about 10-50% by weight EnBAGMA, more preferably about 25-65% by weight, and most preferably about 15-20% by weight, wherein the weight percentages are based on the total weight of the adhesive tie layer.

15 Generally speaking, any of the polymers comprising the multi-layer polymer of the invention herein may additionally contain any number of conventional additives, including fillers, compounding ingredients, antioxidants, antidegradants, tackifiers, processing aids such as lubricants, waxes, plasticizers, and others as would be known to one of skill in the art.

20 Alternatively, in another embodiment of the multi-layer polymer herein, the adhesive tie layer may comprise a two-layer structure, that could be formed by coextrusion or molding prior to joining the first and second outer layers. In this embodiment, just components (c) and (a), as described above, would be used in the adhesive tie layer, each as its own
25 sub-layer. For example, EnBAGMA could be used as component (c) and form one sub-layer, and a copolyester, e.g., a segmented thermoplastic ether-ester, could be used as component (a) and form another sub-layer of the two-layer adhesive tie layer. The adhesive tie layer could then be laminated or coextruded to the first and second outer layers, the
30 EnBAGMA layer contacting the second outer layer and the copolyester contacting the first outer layer.

The invention herein further provides a process for making a multi-layer polymer comprising the step of coextruding the first outer layer, the second outer layer and the adhesive tie layer, as described above. One
35 advantage of the invention herein is that the multi-layer polymer can be easily formed by coextrusion, and avoids multiple-step processing as is the case with most similar multi-layer polymers described in the art. The coextrusion can be accomplished using an insert in the extruder die such as that shown in Figures 1A and 1B, which allows three polymer streams,

of varying thickness, to be extruded into one three-layer structure. The polymer streams will enter through the top of the die insert **40** and exit through the bottom **50**. The die insert has three openings, the first **10** is an opening that can be used for an incoming stream of a first outer layer, the second opening **20** will funnel the incoming stream of the second outer layer, and the third opening **30** will direct the incoming stream of the adhesive tie layer. All three streams will exit the die as one multi-layer polymer. The processing conditions would be known to those skilled in the art.

Additionally, if desired, the multi-layer polymer of the invention herein may also be formed by a process of lamination. In that case, each of the first and second outer layers, and the adhesive tie layer would be individually extruded. The three extruded layers would then be subjected to sufficient heat and pressure to fuse the layers and form a multi-layer polymer. The required heat and pressure would be known to those skilled in the art.

The invention will be further clarified by the following examples, which are intended to be purely exemplary only.

20

EXAMPLES

COEXTRUDABLE ADHESIVE FORMULATIONS

Tables 1 through 7 describe the range of formulations tested, in which a polar resin was adhered to a non-polar, polyolefin substrate.

25

TABLE 1
COEXTRUDABLE ADHESIVE BLENDS
W&P TWIN SCREW (30 mm) SCALE-UP RUNS

5

INGREDIENT (PTS)	1A	1B	1C
HYTREL® 4069 (1)	60	60	60
PP(2)	30	30	30
EBAGMA (3)	10	20	30
MISC.			
PROPERTIES			
TENSILE STR.YLD.(PSI)	1261	1088	1043
(MPa)	8.7	7.5	7.2
ELONG.YLD. (%)	10	11	11
TENSILE STR.BK.(PSI)	1043	1107	1121
(MPa)	7.2	7.6	7.7
ELONG.BK. (%)	57	61	55
MELT IND. (4)	0.2	0.4	0.4
MELT IND. (5)	66	108	112

(1) MI = 0 @ 2.16 KG; 17 @ 21.6 KG (200°C)

(2) PROFAX® 6823 (MI = 0.2)

(3) EP 4934-6 (MI = 15)

10 (4) 200°C, 2160 GR

(5) 200°C, 21.6 KG.

TABLE 2
COEXTRUDABLE ADHESIVE BLENDS
W&P TWIN SCREW (30 mm) SCALE-UP RUNS

5

INGREDIENT (PTS)	2A	2B	2C
HYTREL® 4069 (1)	60	60	60
PP(2)	30	30	30
EGMA (3)	10	20	30
MISC.			
PROPERTIES			
TENSILE STR.YLD.(PSI)	1053	1677	1475
(MPa)	7.3	11.6	10.2
ELONG.YLD. (%)	7	7	7
TENSILE STR.BK.(PSI)	1488	1692	1710
(MPa)	10.3	11.7	11.8
ELONG.BK. (%)	17	52	18
MELT IND. (4)	0.1	0.8	0.6
MELT IND. (5)	54	67	105

(1) MI = 0 @ 2.16 KG; 17 @ 21.6 KG (200°C)

(2) PROFAX® 6823 (MI = 0.2)

(3) EP 4934-8 (MI = 4)

10 (4) 200°C, 2160 GR.

(5) 200°C, 21.6 KG.

TABLE 3
COEXTRUDABLE ADHESIVE BLENDS
W&P TWIN SCREW (30 mm) SCALE-UP RUNS

5

INGREDIENT (PTS)	3A	3B	3C
HYTREL® 4069 (1)	60	60	60
PP(2)	30	30	30
EBAGMA (3)	10	20	30
MISC.			
PROPERTIES			
TENSILE STR.YLD.(PSI)	1110	1556	1000
(MPa)	7.6	10.7	6.9
ELONG.YLD. (%)	9	10	12
TENSILE STR.BK.(PSI)	1157	1520	1008
(MPa)	7.8	10.5	6.9
ELONG.BK. (%)	25	77	68
MELT IND. (4)	0.0	0.0	0.0
MELT IND. (5)	20	15	19

(1) MI = 0 @ 2.16 KG; 17 @ 21.6 KG (200°C)

(2) PROFAX® 6823 (MI = 0.2)

(3) ELVALOY® 4170 (MI = 8)

10 (4) 200°C, 2160 GR.

(5) 200°C, 21.6 KG.

TABLE 4
COEXTRUDABLE ADHESIVE BLENDS
W&P TWIN SCREW (30 mm) SCALE-UP RUNS

5

INGREDIENT (PTS)	4A	4B	4C	4D
HYTREL® 4069	42	42	42	42
PP(1)	38	44	50	56
EGMA (2)	20	20	20	20
MISC.				
PROPERTIES				
TENSILE STR.YLD.(PSI)	2118	2005	1969	2261
(MPa)	14.6	13.8	13.6	15.6
ELONG.YLD. (%)	13	7	7	12
TENSILE STR.BK.(PSI)	1841	2116	2312	1974
(MPa)	12.7	14.6	15.9	13.6
ELONG.BK. (%)	175	28	18	50
MELT IND. (3)	0.3	0.4	0.4	0.3
MELT IND. (4)	60.0	60.0	59.0	46

(1) PROFAX® 6823 (MI = 0.2)

(2) EP 4934-8 (MI = 4)

(3) 200°C, 2160 GR.

10 (4) 200°C, 21.6 KG.

TABLE 5
COEXTRUDABLE ADHESIVE BLENDS
W&P TWIN SCREW (30 mm) SCALE-UP RUNS

5

INGREDIENT (PTS)	5A	5B	5C	5D
HYTREL® 4056	42	42	42	42
PP(1)	38	44	50	56
EGMA (2)	20	20	20	20
MISC.				
PROPERTIES				
TENSILE STR.YLD.(PSI)	2291	1975	2881	2878
(MPa)	15.8	13.6	19.9	19.8
ELONG.YLD. (%)	15	5	18	16
TENSILE STR.BK.(PSI)	1807	2282	2008	2432
(MPa)	12.5	15.7	13.8	16.8
ELONG.BK. (%)	148	25	352	276
MELT IND. (3)	3.2	2.8	2.4	2.2
MELT IND. (4)	169	179	190	159

(1) PROFAX® 6823 (MI = 0.2)

(2) EP 4934-8 (MI = 4)

(3) 200°C, 2160 GR.

10 (4) 200°C, 21.6 KG.

TABLE 6
COEXTRUDABLE ADHESIVE BLENDS
W&P TWIN SCREW (30 mm) SCALE-UP RUNS

5

INGREDIENT (PTS)	6A	6B	6C	6D
HYTREL® 4069	42	42	42	42
PP(1)	38	44	50	56
PP-g-MAH (2)	20	20	20	20
MISC.				
PROPERTIES				
TENSILE STR.YLD.(PSI)	1530	1719	2183	2838
(MPa)	10.5	11.8	15.0	19.6
ELONG.YLD. (%)	4	5	6	11
TENSILE STR.BK.(PSI)	2300	2388	2671	2817
(MPa)	15.8	16.5	18.4	19.4
ELONG.BK. (%)	10	12	24	123
MELT IND. (3)	0.6	0.6	0.5	0.4
MELT IND. (4)	173	161	140	103

- (1) PROFAX® 6823 (MI = 0.2)
 (2) FUSABOND® P 353D (MI = 280)
 (3) 200°C, 2160 GR.
 (4) 200°C, 21.6 KG.

10

TABLE 7
COEXTRUDABLE ADHESIVE BLENDS
W&P TWIN SCREW (30 mm) SCALE-UP RUNS

5

INGREDIENT (PTS)	7A	7B	7C	7D
HYTREL® 4069	42	42	42	42
PP(1)	42	42	42	42
PP-g-MAH (2)	20	20	20	20
PP(3)	14	28	42	56
PROPERTIES				
TENSILE STR.YLD.(PSI)	2837	3045	3097	3190
(MPa)	19.5	21.0	21.3	22.0
ELONG.YLD. (%)	19	17	19	17
TENSILE STR.BK.(PSI)	5238	5021	3006	2639
(MPa)	36.1	34.6	20.7	18.2
ELONG.BK. (%)	857	772	547	468
MELT IND. (4)	0.5	0.5	0.4	0.4
MELT IND. (5)	133	158	95	76

(1) PROFAX® 6823 (MI = 0.2)

(2) FUSABOND® P 353D (MI = 280)

(3) PROFAX® 6823 IN SECOND FEED PORT

10 (4) 200°C, 2160 GR.

(5) 200°C, 21.6 KG.

MELT COMPOUNDING OF THE COEXTRUDABLE ADHESIVES

15 All of the ingredients, including the DuPont Hytrel® copolyester elastomer (dried at 70°C in vacuo), were pellet blended and fed to a 30 mm Werner and Pleiderer co-rotating twin-screw extruder. The extruder consisted of nine barrels totaling 870 mm, and had the screw design as defined in Table 8. The feed port was in the first barrel, and a vacuum port was in barrel 8. A two-hole die, each hole 3/16" (1.27 cm) in diameter,

20 was at the end of barrel 9. As the adhesive melt exited the die, the strands were quenched in a water bath, then cut into pellets. The product was dried (70°C in vacuo) and re-extruded a second time to ensure complete reaction of the functional compatibilizers with the Hytrel®. The temperature profile on the barrels was an uphill profile from 200°C to

25 250°C, resulting in a melt temperature of about 250°C. The screw rpm was 150, and the extrusion rate was 30 lb/hr (14 kg/hr).

TABLE 8
Extruder Screw Design

5

Bushing	Comments		No.
42/42 R	Feed	2	84
42/21 R		1	105
28/28 R		3	189
KB 28 N		2	245
20/10 L		1	255
42/42 R		2	339
KB 28 N		2	395
20/10 L		1	405
42/42 R		2	489
28/28 R		1	517
KB 14 R		1	531
14/14 R		1	545
20/10 L		2	565
42/42 R		4	733
42/21 R		1	754
20/10 L		1	764
28/28 R		3	848
20/10 R		1	858
20/20 R		1	878

****Notation for RH and LH elements is PITCH/LENGTH****

LAP SHEAR TESTING (ASTM D3163-96)

10 Lap shear specimens were prepared using 3 in. long (7.62 cm),
1 in. width (2.54 cm) x 1/8 in. (0.32 cm) thick substrates (i.e., polar and
non-polar outer layers). The polar substrate and non-polar substrate were
laid one upon the other such that they overlapped in a 1 square inch area
(2.54 cm²); a 0.010 in. (0.025 cm) thick adhesive tie layer was used to join
15 them where they overlapped. A shim was placed on the underside of the
top substrate at the end opposite of the overlap.

 Samples were prepared in a preheated press between two
stainless steel plates using 1/8 inch (0.32 cm) shims (as mentioned
above), aligned in such a manner to support the upper substrate and allow
20 the joint/overlap area to be level during pressing. Other shims, of about
0.26 in (0.67 cm) thick were used to allow specimens to be prepared using
contact pressure in the press. Press was preheated to 200°C. After a

press time of 5 minutes, samples were allowed to cool to room temperature before removal from press.

5 Samples were removed from press, the extruded adhesive was trimmed to give a true 1 square inch (2.54 cm²) test area and were left at 23°C, 50% relative humidity overnight. Samples were then tested on an Instron using hand-tightened, non-slip clamps at a crosshead speed of 0.2 in/min (0.5 cm/min). Gauge length was approximately 1.75 inches (4.45 cm).

10 Table 9 summarizes the lap shear values obtained with the adhesives between polyolefins (polypropylene and polyethylene) and a wide range of polar resins. In all cases, no adhesion was observed without the adhesive tie layer.

TABLE 9
CO-EX ADHESIVE LAP SHEAR VALUES (1)

EXAMPLE	POLAR POLYMER	NONPOLAR POLYMER	LAP SHEAR (PSI)	LAP SHEAR (MPa)
1A	PVC (2)	POLYPROPYLENE (3)	353	2.4
1B	"	"	182	1.3
1C	"	"	200	1.4
2A	"	"	292	2.0
2B	"	"	188	1.3
2C	"	"	49	0.3
3A	"	"	105	0.7
3B	"	"	202	1.4
3C	"	"	161	1.1
4A	"	"	100	0.7
4B	"	"	110	0.8
4C	"	"	152	1.0
4D	"	"	148	1.0
5A	"	"	297	2.0
5B	"	"	203	1.4
5C	"	"	349	2.4
5D	"	"	250	1.7
6A	"	"	228	1.6
6B	"	"	105	0.7
6C	"	"	180	1.2
6D	"	"	170	1.2
7A	"	"	185	1.3
7B	"	"	228	1.6
7C	"	"	114	0.8
7D	"	"	65	0.4
6C	POLYCARBONATE (4)	"	75	0.5
"	EVOH (5)	"	230	1.6
"	IONOMER (6)	"	151	1.0
"	PBT (7)	"	80	0.6
"	NYLON 6 (8)	"	284	2.0
"	LCP BLEND (9)	"	104	0.7
"	"	POLYETHYLENE (10)	120	0.8

- 5 (1) 10 MIL (0.025 cm) ADHESIVE FILM BETWEEN TWO POLYMER
BARS (125 MIL (0.32 cm) THICK, EA.), OVERLAPPED BY 1 INCH
(2.54 CM) AND HEATED IN PRESS WITH 0 PRESS. FOR 5 MIN. @
200 °C. CONDITIONED @ 25 °C FOR 22 HRS.

POLYMER BARS PRESSED THIS WAY WITHOUT ADHESIVE FELL
APART

(ZERO LAP SHEAR VALUE).

- (2) GEON® 87416
10 (3) PROFAX® 6823
(4) LEXAN® 134R
(5) SELAR® OH 4416
(6) SURLYN® 8140
(7) CRASTIN® 6129
15 (8) CAPRON® 8202
(9) ZENITE® 400/HYTREL® 4556 (85/15)
(10) SCLAIR® 2909

PEEL STRENGTH TESTING (ASTM D903-98)

- 20 Specimens were cut out of the coextruded laminates in both the
machine direction and the transverse direction. The specimens had a
width of 1 in. (25 mm) and a length of about 6 in. (152 mm). The
thicknesses of the three layers, shown in Table 10, were measured after
the PVC layer was peeled away from the substrate (polypropylene) layer.
25 After conditioning at 50% R.H. and 23°C for 22 hours, the specimens were
mounted into the Instron Tensile Tester with the bottom grips clamped to
the polypropylene substrate and the top grip clamped to the peeled-away,
formerly adjacent, PVC layer.

- This allows an approximate 180° angle of separation of the
30 adhered surfaces. The peel or stripping strength is the average load, per
unit width of bondline, required to separate progressively one surface from
the other over the adhered area.

- The separation rates of 2 inches/min (5.1 cm/min) and 10
inches/min (25.4 cm/min) were used to generate peel strength values in
35 lbs/in (kg/mm) as shown in Table 10.

TABLE 10
PEEL ADHESION VALUES ON COEXTRUDED SHEET

EX.	LAYER THICKNESSES (MILS/mm)				ADHESION (3)			
	PP (1)	ADH.	PVC (2)	2"/MIN	10"/MIN.			
				(5.1 cm/min)	(25.4 cm/min)			
				lbs/in	kg/mm	lbs/in	kg/mm	
4A	71/1.8	8/0.20	9/0.23	2-6	0.04-0.11	3-8	0.05-0.14	
4B	74/1.9	7/0.18	9/0.23	2-6	0.04-0.11	4-6	0.07-0.11	
4C	77/2.0	6/0.15	7/0.18	4-5	0.07-0.09	4-7	0.07-0.13	
4D	77/2.0	6/0.15	3/0.08	2-3	0.04-0.05	3-5	0.05-0.09	
6A	73/1.9	6/0.15	3/0.08	1-2	0.03-0.04	3-4	0.05-0.07	
6B	74/1.9	6/0.15	2/0.05 1	1-6	0.02-0.11	3-7	0.05-0.13	
6C	74/1.9	7/0.18	2/0.05 1	4-6	0.07-0.11	5-8	0.09-0.14	
6D	70/1.8	1/0.02	3/0.08	3-5	0.05-0.09	6-9	0.11-0.13	
7A	74/1.9	8/0.20	4/0.10	3-4	0.05-0.07	6-7	0.11-0.13	
7B	73/1.9	8/0.20	3/0.08	4-7	0.07-0.13	5	0.09	
7C	74/1.9	9/0.23	3/0.08	5	0.09	6	0.11	
7D	71/1.8	9/0.23	3/0.08	3-4	0.05-0.07	4-6	0.07-0.11	

5

(1) PROFAX® 6823

(2) GEON® 83974 BROWN 3830

(3) 180 °, LBS./IN.(kg/mm): RANGE OF VALUES ACROSS SHEET
WIDTH INCLUDING MD AND TD PULLS

10

1 inch (2.54 cm) sample

CONTROL WITHOUT ADHESIVE HAS NO ADHESION (FALLS APART)

COEXTRUSION PROCESS

General Layout

5 The following explains the coextrusion process used to produce
coextruded samples for the examples. Three extruders were coupled via
transfer lines to a feedblock which in turn was connected to a flat film die.
The coextruded film was fed to a three-roll stack consisting of a pair of nip-
rolls followed by a casting roll. This, in turn, was followed by haul-off rolls
10 consisting of two rubber nip-rolls followed by a wind-up roll for collecting
final product.

Extruder A

 This extruder was used to melt and feed the non-polar,
polyolefin resin. It was manufactured by Killion Extruders, Inc., and has a
15 screw 36 inches (91 cm) in length and 1.5 inches (3.81 cm) in diameter. A
mixing section of 20 inches (51 cm) in length is incorporated in the screw.

Extruder B

 This extruder, from the same manufacturer of Extruder A, is
equipped with a screw that is 24 inches (61 cm) in length and 1 inch (2.54
20 cm) in diameter and is of general purpose screw design. Extruder B was
used to melt and feed the coextrudable adhesives.

Extruder C

 This extruder is also of the same manufacturer and was
25 equipped with a screw that is 30 inches (76 cm) in length and 1.25 inches
(3.2 cm) in diameter. This screw is also a general purpose screw and was
used to melt and feed the polar, e.g., PVC resin.

Feedblock

 The coextrusion feedblock, into which the three melt streams
30 converge, is equipped with an insert that brings the three melt streams
together with the PVC being the top layer, the adhesive the middle layer,
and the polyolefin the bottom layer. Figures 1A and 1B show the design of
this insert.

Die

35 The die was manufactured by Extrusion Dies, Inc., and is of the
"coat-hanger" design with adjustable lips and is 14 inches (35.6 cm) wide.

Processing Conditions

Extruder A was run at 131 rpm with barrel temperature set to generate a polypropylene melt temperature of 200 to 212°C. Extruder B was run at 30-36 rpm with barrel temperature set to generate an adhesive melt temperature of 197 to 209°C. Extruder C was run at 31 to 37 rpm with barrel temperature set to generate a PVC melt temperature of 198 to 203°C. The transfer lines were set at 195-210°C, and the die was set at 195°C. A product take-off rate of 1.7 feet per minute (52 cm/min) was used.

Product Properties

Table 10 summarizes the properties of the three-layer films that were produced from the various coextruded samples. Good adhesion was obtained in all examples relative to the control which showed no adhesion without the adhesives.